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# Low-temperature sintering and microwave dielectric properties of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with ZnB<sub>2</sub>O<sub>4</sub> glass

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#### Abstract

The Influence of  $ZnB_2O_4$  glass addition on the sintering temperature and microwave dielectric properties of  $Ba_5Nb_4O_{15}$  has been investigated using dilatometry, X-ray diffraction, scanning electron microscopy and network analyzer. It was found that a small amount of glass addition to  $Ba_5Nb_4O_{15}$  lowered the sintering temperature from 1400 to 900 °C. The reduced sintering temperature was attributed to the formation of  $ZnB_2O_4$ liquid phase and  $B_2O_3$ -rich liquid phases such as  $Ba_3B_2O_6$ . The  $Ba_5Nb_4O_{15}$  ceramics with  $ZnB_2O_4$  glass, sintered at a low temperature, exhibited good microwave dielectric characteristics, i.e., a quality factor ( $Q \times f$ ) = 12,100 GHz, a relative dielectric constant ( $\varepsilon_r$ ) = 40, a temperature coefficient of resonant frequency ( $\tau_f$ ) = 48 ppm/°C. The dielectric properties were discussed in terms of the densification of specimens and the influence of glassy phases such as  $Ba_3B_2O_6$  and  $ZnB_2O_4$ .

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# 1. Introduction

Multilayer microwave components have been investigated to miniaturize resonant devices for volume efficiency. To be a useful material for incorporation into multilayer type elements, dielectrics must be capable of being sintered along with electrodes, a process known as cofiring. In multilayer structures, glasses having a low melting point are frequently utilized. Consequently, the dielectrics can be cofired with conducting layers such as silver thick films whose melting point is 961 °C. There have been three approaches to reduce the sintering temperature of the dielectric ceramics: addition of glass having a low meltingtemperature, chemical processing, and utilization of ultra-fine particles for raw materials. Liquid-phase sintering with glass additives is the least expensive process among the described method. However, in order to sinter the microwave dielectric ceramics at a low temperature, 20-30 wt% of glass should be contained indispensably, thus the dielectric property such as a quality factor and a relative dielectric constant ( $\varepsilon_r$ ) is diminished significantly.<sup>1</sup> In this sense, the study on searching the suitable glass-dielectric ceramics compositions and on optimizing the

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sintering conditions for the low temperature sintering and good dielectric properties is essential.

The dielectric properties of a Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> system have been widely investigated and it has been found to be a useful material in microwave communication applications.<sup>2,3</sup> The microwave dielectric properties of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> have been reported by Sreemoolandgna et al.<sup>4</sup> More recently, Ratheesh et al. measured the microwave dielectric properties of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> using the whispering gallery mode technique and reported it's outstanding dielectric properties (quality factor = 53,000 GHz at 16 GHz,  $\varepsilon_r = 40$ , and  $\tau_f = 78 \text{ ppm/}^\circ \text{C}$ ).<sup>5</sup>

However, the sintering temperature of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> is above 1400 °C, which is too high to be applicable to multilayer microwave components.<sup>4,5</sup> However, the influence of glass addition on the firing temperature and dielectric properties of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> has not been studied. For the first time, a small amount of ZnB<sub>2</sub>O<sub>4</sub> glass was added to lower the sintering temperature of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> to 900 °C in the present work. The microwave dielectric properties of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>-glass composites sintered at a low temperature were also studied.

### 2. Experimental procedure

The glass was prepared by mixing molar ratio of 1:1 of ZnO (Cerac, Milwaukee, WI) and B<sub>2</sub>O<sub>3</sub>(High Purity Chemical Labo-

ratory, Saitama, Japan) in a batch size to yield 30 g of glass. The glass filled in an uncovered Pt crucible was melted at  $1000 \,^{\circ}$ C. The melt was homogenized for 1 h and quenched on steel plates.

The Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> powders were synthesized by conventional mixed oxide methods: BaCO<sub>3</sub> (Cerac, Milwaukee, WI) and Nb<sub>2</sub>O<sub>5</sub> (High Purity Chemical Laboratory, Saitama, Japan) were mixed homogeneously and calcined at 1100 °C for 2 h. The calcined powders containing a proper amount of ZnB<sub>2</sub>O<sub>4</sub> glass were ball-milled for 48 h using ethanol solvent. The milled powders were then dried, granulated, and pressed at 1000 kg/cm<sup>2</sup> to yield several disk-type pellets (8 mm in diameter and 3 mm in thickness). The pellets were sintered at 850–950 °C for 2 h with a heating rate of 5 °C/min.

Shrinkage of the specimens during heat treatment was measured using a horizontal loading dilatometer with alumina rams and boats (Model DIL402C, Netzsch Instruments, Germany). The bulk density of the sintered samples was determined by the Archimedes method. Polished and thermally etched surfaces of sintered specimens were examined using field emission scanning electron microscopy (FESEM: Model JSM6330F, Japan Electronic Optics Laboratory, Japan). The crystal structures of sintered specimens were investigated using X-ray powder diffraction (Model M18XHF, Macscience Instruments, Japan). The microwave dielectric properties of sintered samples were measured at x-band frequencies (8–12 GHz) using a network analyzer (Model HP8720C, Hewlett-Packard, Palo Alto, CA).

#### 3. Results and discussion

# 3.1. Sintering behavior of $Ba_5Nb_4O_{15}$ with $ZnB_2O_4$ glass additions

Fig. 1(a) shows the change in shrinkage of  $Ba_5Nb_4O_{15}$ ceramic with varying amount of ZnB<sub>2</sub>O<sub>4</sub> glass. The results demonstrate that the onset temperature of shrinkage is lowered by the small addition of ZnB2O4 glass. The shrinkage of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> without ZnB<sub>2</sub>O<sub>4</sub> glass does not occur as rapidly as that with the glass. It is noteworthy that the densification of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.5 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass addition begins below 800 °C and that the shrinkage reaches a maximum value at approximately 900 °C. For Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 3 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass addition, the shrinkage begins at ~600 °C but the ultimate shrinkage is lower than that of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.5 wt% ZnB<sub>2</sub>O<sub>4</sub> glass addition. Fig. 1(b) shows a typical result of thermal mechanical analysis (TMA) measurement of ZnB<sub>2</sub>O<sub>4</sub> glass.  $ZnB_2O_4$  glass has a low softening temperature  $(T_s) = 587 \degree C$  and begins to melt above  $T_s$ . This result supports that the low temperature densification originates from the formation of liquid phase.

The bulk density and relative theoretical density of  $Ba_5Nb_4O_{15}$  specimens with 0.1–3 wt% of  $ZnB_2O_4$  glass additions are plotted in Fig. 2. The density sharply increased with increasing  $ZnB_2O_4$  glass additions. The bulk density of specimens with the addition of 0.3–1.0 wt% of  $ZnB_2O_4$  glass, sintered at 900 °C for 2 h, increased to 96% of the theoretical density compared with that of  $Ba_5Nb_4O_{15}$  (6.293 g/cm<sup>3</sup>). These results demonstrate that low-temperature sintering of  $Ba_5Nb_4O_{15}$  is successfully achieved by addition of  $ZnB_2O_4$  glass. However,

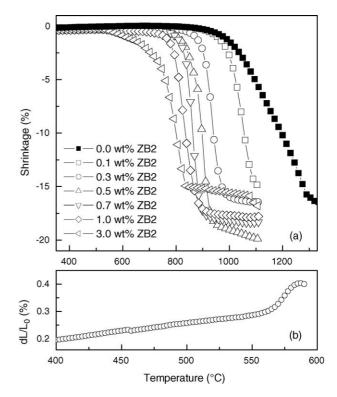


Fig. 1. (a) Shrinkage of the  $Ba_5Nb_4O_{15}$  samples with 0.1–3 wt% ZnB<sub>2</sub>O<sub>4</sub> glass additions and (b) TMA curve of ZnB<sub>2</sub>O<sub>4</sub> glass as a function of temperature.

the density of the specimen with the addition of above 3.0 wt% of  $\text{ZnB}_2\text{O}_4$  glass slightly decreased.

Scanning electron micrographs of  $Ba_5Nb_4O_{15}$  with various amounts of  $ZnB_2O_4$  glass sintered at 900 °C for 2 h, are shown in Fig. 3. The sintered  $Ba_5Nb_4O_{15}$  specimen containing 0.3 wt% of  $ZnB_2O_4$  glass has elongated grains with a small grain size (1–2  $\mu$ m) as previously reported by Sreemoolanadhan et al.<sup>4</sup> The SEM micrographs show that the sintered specimens with 0.3–1.0 wt% of  $ZnB_2O_4$  glass have dense microstructures

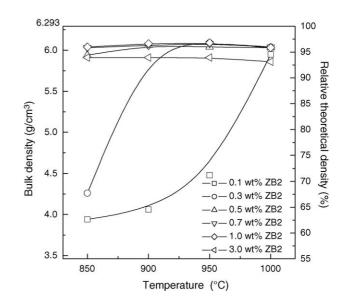


Fig. 2. Bulk density and relative theoretical densities of the  $Ba_5Nb_4O_{15}$  samples with 0.1–3 wt% ZnB<sub>2</sub>O<sub>4</sub> glass additions as a function of sintering temperatures.

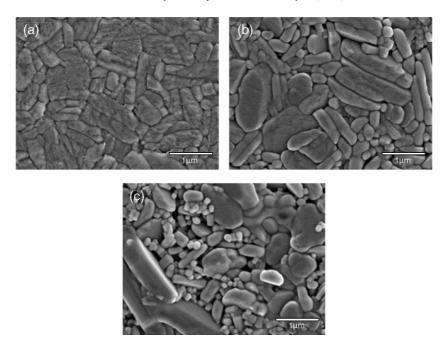


Fig. 3. Scanning electron micrographs of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> samples sintered at 900 °C for 2 h with (a) 0.3, (b) 3, (c) 10 wt% ZnB<sub>2</sub>O<sub>4</sub> glass addition.

(Fig. 3(a)). However, as shown in Fig. 3(b) and (c), excess addition of  $ZnB_2O_4$  glass (above 3 wt%) induces an abnormal grain growth severely and thereafter results in less dense microstructures, which is in a good agreement with the change in the density as a function of glass contents. The average size of abnormal elongated grains is larger than 5  $\mu$ m. This abnormal grain growth indicates that the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>–ZnB<sub>2</sub>O<sub>4</sub> glass composite involves with liquid-phase sintering.

Fig. 4 shows XRD patterns of  $Ba_5Nb_4O_{15}$  specimens with 0.1–10 wt% ZnB<sub>2</sub>O<sub>4</sub> glass sintered at 900 °C. The crystalline ZnB<sub>2</sub>O<sub>4</sub> phase is found to exist in the XRD pattern of the speci-

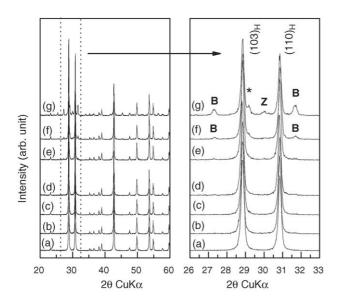


Fig. 4. XRD patterns of the  $Ba_5Nb_4O_{15}$  samples with *x* wt% ZnB<sub>2</sub>O<sub>4</sub> glass addition sintered at 900 °C for 2 h. ((\*) ZnB<sub>2</sub>O<sub>4</sub>, B:  $Ba_3B_2O_6$ , Z: ZnNb<sub>2</sub>O<sub>6</sub>), (*x* = (a) 0.1, (b) 0.3, (c) 0.5, (d) 0.7, (e) 1, (f) 3, (g) 10).

mens containing  $ZnB_2O_4$  glass. Above the 0.5 wt% of glass addition, the trace of secondary phases such as crystalline  $Ba_3B_2O_6$  phase is observed in the XRD patterns and the intensity increases with the amount of  $ZnB_2O_4$  glass addition. The  $ZnNb_2O_6$  phase is found at an excess addition of  $ZnB_2O_4$  glass, also.

The  $Ba_3B_2O_6$  phase would enhance the densification of  $Ba_5Nb_4O_{15}$ . In the phase diagram of  $BaO-B_2O_3$ , the  $BaB_8O_{13}-BaB_4O_7$ ,  $BaB_4O_7-BaB_2O_4$ ,  $BaB_2O_4-Ba_3B_2O_6$ eutectics exist as low as 859, 889, 905 °C.<sup>6</sup> The formation of a  $B_2O_3$ -rich liquid phase containing  $Ba_3B_2O_6$  can assist in the densification of  $Ba_5Nb_4O_{15}$ .

# 3.2. Microwave properties of $Ba_5Nb_4O_{15}$ sintered at a low temperature

In the present work, the  $Ba_5Nb_4O_{15}$  specimen without  $ZnB_2O_3$  glass shows a  $\varepsilon_r$  of 40.8, a quality factor of 50,000 GHz, and a temperature coefficient of resonant frequency ( $\tau_f$ ) of 50 ppm/°C.

Fig. 5(a) shows  $\varepsilon_r$  of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> specimens sintered at 900 °C for 2 h as a function of ZnB<sub>2</sub>O<sub>4</sub> glass content. Relative dielectric constant ( $\varepsilon_r$ ) of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.1 wt% ZnB<sub>2</sub>O<sub>4</sub> glass is 19.6 which is attributed to a low bulk density as shown in Fig. 2. However,  $\varepsilon_r$  of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.3 wt% ZnB<sub>2</sub>O<sub>4</sub> glass is 40.7, same to that of pure Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> specimen. Excess additions of ZnB<sub>2</sub>O<sub>4</sub> glass (above 0.3 wt%) cause a slight decrease of  $\varepsilon_r$ , which can be interpreted with the dielectric constants of the secondary phases such as ZnB<sub>2</sub>O<sub>4</sub>, ZnNb<sub>2</sub>O<sub>6</sub>, and Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> which were detected in the XRD analysis. Lee et al. reported that ZnNb<sub>2</sub>O<sub>6</sub> had a low  $\varepsilon_r$  of 25.<sup>7</sup> Also, Wu et al. made a systematic study of dielectric properties of ZnB<sub>2</sub>O<sub>4</sub> glass system at microwave frequencies.<sup>8</sup> According to their studies, ZnO–B<sub>2</sub>O<sub>3</sub> glass with molar ratio of 1:1 showed a low  $\varepsilon_r$  of 6.88. Although

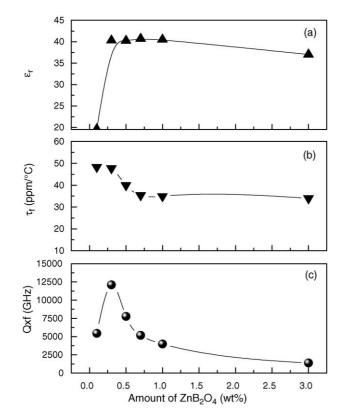


Fig. 5. Microwave dielectric properties of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> samples sintered at 900 °C for 2 h as a function of ZnB<sub>2</sub>O<sub>4</sub> glass: (a) relative dielectric constant ( $\varepsilon_r$ ), temperature coefficient of resonant frequency ( $\tau_f$ ), (c) quality factor ( $Q \times f$ ).

the dielectric properties of crystalline Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> is not fully characterized, BaO–B<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass with a molar ratio of 5:4:1 exhibited a low  $\varepsilon_r$  of 9.15. Therefore, it can be suggested that slight reduction of  $\varepsilon_r$  observed in the low-temperature sintered Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> can be attributed to the low  $\varepsilon_r$  of secondary phases, which were slightly contained in Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> specimens.

Fig. 5(b) shows  $\tau_f$  of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> samples sintered at 900 °C for 2 h as a function of ZnB<sub>2</sub>O<sub>4</sub> glass content.  $\tau_f$  decreased slightly to 34 ppm/°C with the 3 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass addition in comparison with 50 ppm/°C for pure BaNb<sub>4</sub>O<sub>15</sub>. Secondary phases having a small  $\tau_f$  such as ZnB<sub>2</sub>O<sub>4</sub> (-10 ppm/°C) and ZnNb<sub>2</sub>O<sub>6</sub> (-56 ppm/°C) would contribute to the slight decrease in  $\tau_f$  of ZnB<sub>2</sub>O<sub>4</sub> glass-added Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> system, also.

The quality factors of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> specimens, sintered at 900 °C for 2 h, were plotted in Fig. 5(b) as a function of ZnB<sub>2</sub>O<sub>4</sub> glass content. The small quality factor (5500 GHz) of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.1 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass is correlated with the poor densification, which is same to the case in dielectric constant. The quality factor of the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> with 0.3 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass showed a maximum value, 12,100 GHz. However, further addition of ZnB<sub>2</sub>O<sub>4</sub> glass diminished the quality factor, significantly. The change in quality factor corresponds to the formation of secondary phases as shown in Fig. 4. It is notable that the onset point of secondary phase is same to that of decrease in quality factor. The trace of Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> was found at 0.5 wt% of ZnB<sub>2</sub>O<sub>4</sub> glass addition and the quality factor diminished, simultaneously. Considering that the bulk densities of specimens with 0.3-1.0 wt% of glass addition are almost same, the secondary phases critically deteriorate the quality factor. The similar behavior was reported by Takada et al. They reported that sintering studies and microwave property measurements were performed on BaO–TiO<sub>2</sub>–WO<sub>3</sub> ceramics with additions of either 5ZnO–2B<sub>2</sub>O<sub>3</sub> glass.<sup>1</sup> Their results showed that the density of BaO–4TiO<sub>2</sub>–0.1WO<sub>3</sub> ceramics reached 98% of the theoretical density at sintering temperature of 900 °C, but the quality factor of those specimens significantly decreased. The significant deterioration of quality factor in Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> specimens with an excess addition of ZnB<sub>2</sub>O<sub>4</sub> glass is related to the formation of secondary phases having the lower quality factors, i.e., ZnB<sub>2</sub>O<sub>4</sub> (1,733 GHz) and Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> (1,221 GHz).

## 4. Conclusion

It was found that a small addition of ZnB<sub>2</sub>O<sub>4</sub> glass to Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> enabled a reduction in sintering temperature from 1400–900 °C. ZnB<sub>2</sub>O<sub>4</sub> glass with  $\sim$ 587 °C of softening point  $(T_s)$ , starts to melt at approximately 600 °C. During sintering of Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>-ZnB<sub>2</sub>O<sub>4</sub> glass composites, Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> was found to react with ZnB<sub>2</sub>O<sub>4</sub> glass, primarily forming Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> crystalline phase and ZnNb<sub>2</sub>O<sub>6</sub>. The low temperature sintering was suggested to originate from the formation B<sub>2</sub>O<sub>3</sub>-rich liquid phases including Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> as well as ZnB<sub>2</sub>O<sub>4</sub> liquid phase. Moreover, the secondary phases such as Ba<sub>3</sub>B<sub>2</sub>O<sub>6</sub> were found to critically influence the microwave dielectric properties of low temperature sintered Ba5Nb4O15. As a result of optimizing the glass addition content (0.3 wt%), the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>-ZnB<sub>2</sub>O<sub>4</sub> glass composite, sintered at a low temperature, 900 °C, showed a dense structure and outstanding dielectric properties: quality factor = 12,100 GHz,  $\varepsilon_r$  = 40,  $\tau_f$  = 48 ppm/°C. These results demonstrate that the Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>–ZnB<sub>2</sub>O<sub>4</sub> glass composite is a promising candidate for low temperature cofired ceramics (LTCC).

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